13 OCTOBER 2025

ALLANITE RARE EARTHS PROCESSING BREAKTHROUGH: SUCCESSFUL COMPLETION OF IMPURITY REMOVAL NEUTRALIZATION TESTS

Highlights

- **Impurity Removal Metallurgical Tests Yield Allanite Rare Earths Processing Breakthrough:**
  - Impurity removal is one of the last steps in the hydrometallurgical processing of rare earths elements ("REE") and is performed to remove non-REE minerals from the leach liquor prior to solvent extraction and separation (i.e. the final steps before producing rare earths oxide). Historically, this has been a challenging step for processing allanite-based REEs, like Halleck Creek's ore, as the mineral typically produces unwanted byproducts such as gypsum and silica gel, resulting in additional and difficult processing steps to remove them.
  - In a recent and extensive impurity removal test program on Halleck Creek ore minimal gypsum and silica gel were formed during the process, which points to immense operating benefits, including but not limited to the reduction of rare earths yield loss and fewer processing steps resulting in potentially lower capital and operating expenses.
  - **<u>These results de-risk what has historically been a material technical and economic hurdle in the processing of allanite-based rare earths elements (i.e. Halleck Creek's ore) and represent a major milestone in unlocking Halleck Creek's vast REE supply potential.</u>**
- **Adverse Elements removed from Leachate Solutions**
  - Effectively 100% of iron, titanium and other deleterious elements precipitated from Leachate Solutions
  - Over 99% of silica and aluminum precipitated from Leachate Solutions
- **Magnesium Oxide (MgO) chosen as the optimal neutralizing reagent**

American Rare Earths (**ASX: ARR | OTCQX: ARRNF | ADR: AMRRY) ("ARR"** or the **"Company"**) has successfully completed a critical stage in its mineral processing program, the first phase of impurity removal testing, with highly encouraging results. This milestone confirms that key contaminants like iron, aluminum, silica and others can be effectively removed from Halleck Creek ore, paving the way for efficient rare earths extraction. Importantly, the tests showed minimal formation of problematic by-products like gypsum and silica gel, a common challenge in processing allanite-based rare earths elements.

SGS completed the neutralization testing at their laboratory in Lakefield, Ontario, Canada. The results will be a key input in the hydrometallurgical processing portion of the Pre-Feasibility Study flowsheet. The objective of impurity removal is to remove deleterious elements (such as iron, aluminum, silica and others) from the rare earth elements ("REE") in leachate solutions. Impurity removal is the next processing step after leaching[1] and is accomplished by adding reagents to neutralize the leach liquor at

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[1] See ASX Release dated 16 July 2025

specific pH ranges. At different pH levels, the various deleterious elements precipitate out and are removed from the leach solution by filtration. Throughout this robust testing program, ARR's third-party lab, SGS tested various reagents over various pH ranges to determine the optimal conditions for Halleck Creek. The next step of hydrometallurgical testing will be to create a mixed rare earth oxide, which is a precursor to solvent extraction and creating individual, separated oxides used in permanent magnets.

Six potential neutralizing agents were tested on REE enriched leach solutions. Magnesium oxide (MgO) and magnesium carbonate ($MgCO_3$) yielded the best results. Looking forward, magnesium oxide is a more cost-effective reagent than magnesium carbonate and was selected as the optimal neutralizing reagent for the mineral processing flow-sheet.

Given allanite (i.e. REE host mineral) is rich in calcium and silica, it was anticipated that gypsum (i.e. calcium sulfate) and/or silica gel might form during the impurity removal test program. The solutions neutralized with MgO formed few of these unwanted products, which will likely yield significant operational benefits, including but not limited to reduction of REE yield loss, fewer additional processing steps and lower capital and operating expenses. Historically, the formation of these products has proven to be a material technical and economic hurdle to overcome in the processing of allanite-based rare earths.

The primary neutralization using 15% MgO for 2 hours at 75°C and pH 3.15 (i.e. test PN12) removed 99.8% iron, 89.0% silica, 92.9% thorium, and 99.4% titanium with an average REE loss for light ("LREE") and heavy rare earths ("HREE")[2] of 0.6% and 0.8%, respectively. Furthermore, 40.5% aluminum was removed during primary neutralization, which is greater than anticipated. The secondary neutralization (i.e. test SN2) using between 5% and 10% MgO for 2 hours at 75°C and pH of 5.0 removed 99.4% Iron, 96.3% aluminum, 71.0% silica, 98.9% Thorium, and 95.6% Titanium from what was left in the solution after the primary neutralization. An average of 7.6% of LREE and 16.7% of the HREE were precipitated during secondary neutralization. Our technical consultants recommend recycling the solids from secondary neutralization back to leaching to capture the REE for reprocessing.

Why it matters?

Impurity removal testing was performed on leachate solutions prepared from mineral concentrate material collected from four core holes at Halleck Creek as previously released[3]. The main goal of the neutralization tests is to remove impurities (i.e. non-rare earth elements) from the leach liquor containing the dissolved REEs through precipitation, while minimizing the loss of REEs through co-precipitating alongside the impurities.

Impurity removal is a key step in producing rare earth products from Halleck Creek ore. The tests were completed ahead of schedule and the data received will be used in the mineral processing flow-sheet design for the upcoming Pre-Feasibility Study ("PFS"). Removing non-REE elements from leachate solutions enables the REE to be extracted from solution via solvent extraction and ultimately produce separated rare earth oxides (precursors for rare earths permanent magnets). Iron, silica, aluminum and other deleterious elements can contaminate the solvent extraction process and must be removed from the leachate beforehand. The impurity removal testing demonstrated that these elements can removed

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[2] Light Rare Earths include La, Ce, Pr and Nd. Heavy rare earths include Sm, Eu, Gd, Tb and Dy.

[3] ASX Release 16 July 2025

from leachate solutions thus providing a highly enriched and clean solution for rare earth product refining. The successful completion of these tests is a major metallurgical processing milestone for Halleck Creek's allanite based rare earths.

Metallurgical Testing Next Steps

- Hydrometallurgical testing is nearing completion.
- SGS will then create a mixed rare earth oxalate by precipitating the REE with oxalic acid.
- The mixed rare earth oxalate will be calcined to create a mixed rare earth oxide (i.e. the precursor to separated rare earth oxides).
- The mixed rare earth oxide will be re-leached. Cerium oxide is insoluble in the leach reagent and will be filtered out of the new leachate solution. The final leachate solution is then ready for future solvent extraction testing.

ARR expects these final tests to be completed before the end of the year. In parallel, bulk samples from the CSM test pit have been delivered to Fl Smidth, Loesche and Weir (Corem) for comminution optimisation testing which is currently in progress. These results will be reported to the market as soon as they are complete.

Additional Technical Details

Impurity removal testing was performed on leachate solutions prepared from mineral concentrate material collected from four core holes at Halleck Creek as previously released[4].

In general, iron, silica, and thorium become insoluble in solutions with pH values between 2.75 and 3.25 and precipitated out. REEs generally remain in solution at these same pH ranges. Therefore, by raising the pH of the leachate solution, iron, silica and thorium can be precipitated and removed via filtration while REE stays in solution. This is called primary neutralization.

Aluminum and uranium generally become insoluble in solutions with pH values between 4.5 and 6.0. REE generally remain in solution at these same pH ranges. Increasing pH of the solution in secondary neutralization, iron, thorium, aluminum, and uranium can be precipitated and removed via filtration from solution.

By performing impurity removal in two neutralization steps, fewer REE are precipitated because the chemical reactions are more controlled. If the pH of the leachate solution was suddenly increased to above 3.5, losses of REE through co-precipitation would occur as a result.

Different reagents react differently with chemical elements in various leachate solutions. SGS performed a comprehensive series of tests to determine which chemical reagents and pH values are most effective on Halleck Creek leachate solutions.

Reagent Selection

SGS, in Lakefield Ontario, tested six leach liquor neutralization reagents for impurity removal from leach solutions including:

- Magnesium oxide (MgO)
- Magnesium carbonate ($MgCO_3$)
- Sodium hydroxide ($NaOH$)
- Sodium carbonate (soda ash)
- Limestone (calcium carbonate)
- Lime (CaO)

SGS performed pH profile testing over a range of pH values from 2.5, 3.0, 3.5, 4.0, and 4.5 for each reagent, PN1 through PN 6. Table 1 and Figure 1, and Figure 2 summarize the results of the tests. The tests were all performed at 75°C and the reagent strengths varied between reagent types.

Magnesium oxide and magnesium carbonate performed well in testing. Iron (Fe) and thorium (Th) were precipitated at high levels, while REE precipitation was low across the pH ranges tested. Figure 1 below shows that at pH less than 3.5, Nd and Dy have minimal precipitation. Conversely, Figure 2 shows that Fe and Th have over 80% precipitation when pH is less than 3.5.

The limestone and lime performed poorly because they precipitated gypsum and co-precipitated rare earth elements from the leach solution.

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[4] ASX Release 16 July 2025

The sodium hydroxide and soda ash also performed poorly because they formed sodium/rare earth double salts and precipitated rare earth elements from the leach solution.

Conversely, to the calcium- and sodium-based reagents, solutions neutralized by MgO did not exhibit formation of gypsum or silica gel during the course of testing. SGS and Tetra tech attribute this to the reagent type, dilution, the temperature of the solutions, and the short residence times of testing.

Table 1 – pH Profile Testing Results for Primary Neutralization by Reagent Type and pH Range

Primary Neutralization

Test ID	**PN1**	**PN2**	**PN3**	**PN4**	**PN5**	**PN6**
Feed	Comp Bench AL Filtrate	Comp Bench AL Filtrate	Comp Bench AL Filtrate	Comp Bench AL Filtrate	Comp Bench AL Filtrate	Comp Bench AL Filtrate
Reagent	MgO	MgCO3	NaOH	Na2CO3	CaO*	CaCO3*
Reagent Strength (% w/w)	15%	15%	10%	10%	15%	20%
pH Target	2.5 - 4.5	2.5 - 4.5	2.5 - 4.5	2.5 - 4.5	2.5 - 4.5	2.5 - 4.5
Retention Time (h)[1]	1	1	1	1	1	1
Temperature (°C)	75	75	75	75	75	75
Reagent Addition (kg/m^3)	19	38	29	37	24	39
Est. Filtration Rate (kg/m^{2}h)	8.4	7.3	4.3	3.1	35.9	29.9

[1] for each pH target, as applicable

* client supplied sample

Precipitation (%)[1]	**PN1**	**PN2**	**PN3**	**PN4**	**PN5**	**PN6**
LREE Avg	5.3	21.6	60.6	74.1	68.0	71.6
HREE Avg	12.8	42.2	57.2	65.4	81.6	78.8
Th	90.3	97.5	94.4	92.8	99.1	98.1
U	52.0	84.4	72.7	77.8	98.4	96.4
Si	95.2	96.3	96.5	96.2	98.0	98.0
Al	80.4	92.0	82.1	81.3	93.2	89.3
Fe	87.2	99.5	96.9	96.0	98.9	98.1
Mg	0.1	0.1	2.1	3.3	21.5	10.3
Ca	0.5	0.7	4.1	11.2	96.9	96.7
Na	4.7	0.8	0.2	1.0	35.0	50.2
K	1.2	0.7	2.0	3.5	7.9	14.8
Ti	99.9	100.0	100.0	100.0	100.0	100.0
P	92.4	91.2	92.6	92.6	93.4	93.4
Mn	1.2	1.6	1.5	1.5	6.8	6.5

[1] overall, potentially skewed by partial sampling

Figure 1 – pH Profiling Charts for Nd and Dy

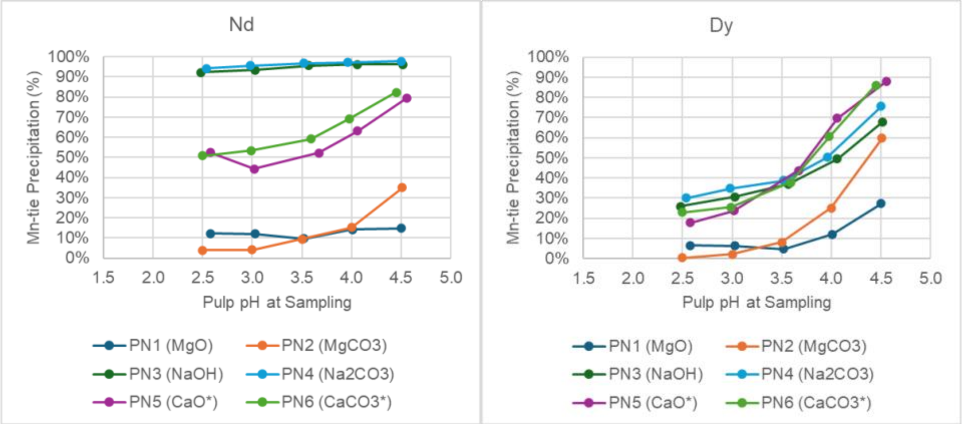
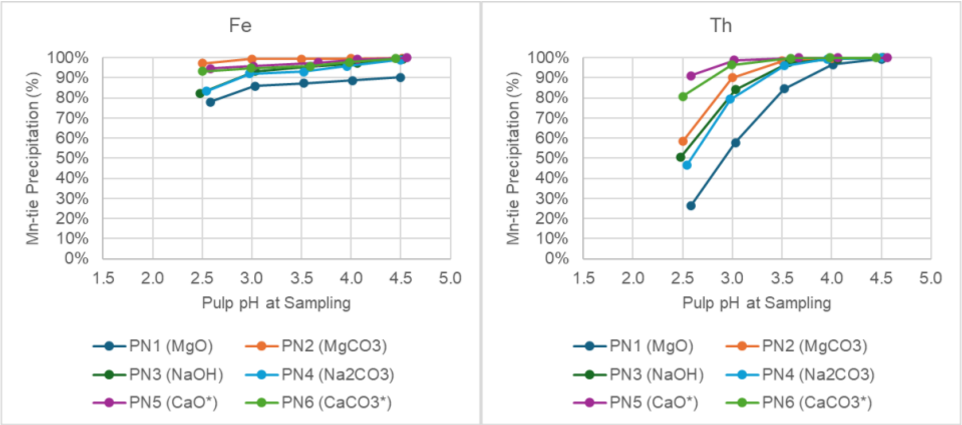


Figure 2 - pH Profile Charts for Fe and Th



Primary Neutralization ("PN")

The pH profile tests clearly showed that MgO and $MgCO_3$ were superior to the other reagents for impurity removal and rare earth recovery. SGS compared MgO and MgCO3 for primary neutralization at a static pH of 3.25. The tests results were very similar. Tetra Tech engineers determined that MgO is a more cost-effective reagent than MgCO3 when considering dosage rates and the cost of the reagents. Therefore, MgO was selected as the reagent for primary neutralization. It is important to note that both MgO and $MgCO_3$ did not form gypsum or silica gel in the neutralization process. Historically, the formation of these products has proven to be a material technical and economic hurdle to overcome in the processing of allanite-based rare earths.

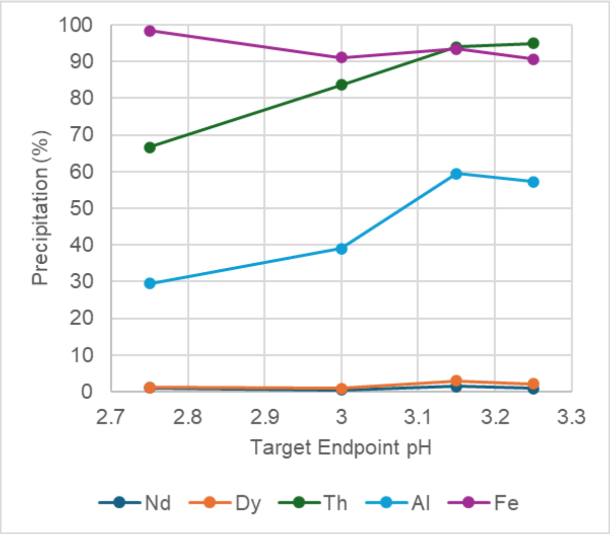
With the selection of MgO as the neutralization reagent, SGS performed detailed pH endpoint tests for pH ranges from 2.75, 3.0, and 3.25, tests PN7, PN9, and PN10, respectively, see Table 3 and Figure 3. These tests indicate that a target pH of 3.15 is the optimal pH for primary neutralization. Test PN13 was then performed using a pH of 3.15, confirming this value.

Table 2 – Endpoint pH Comparison of Primary Neutralization for MgO

Test ID	**PN10**	**PN9**	**PN13**	**PN7**
Feed	Comp Bench AL Filtrate	Comp Bench AL Filtrate	AL22 Filtrate	Comp Bench AL Filtrate
Reagent	MgO	MgO	MgO	MgO
Reagent Strength (% w/w)	15%	15%	15%	15%
pH Target	2.75	3.00	3.15	3.25
Retention Time (h)[1]	3	3	1	2
Temperature (°C)	75	75	75	75
Reagent Addition (kg/m^3)	14.2	12.5	28	15
Est. Filtration Rate (kg/m^2h)	4.5	4.4	0.8	1.9

Precipitation (%)	**PN10**	**PN9**	**PN13**	**PN7**
LREE Avg	0.9	0.4	1.2	0.6
HREE Avg	1.0	0.6	2.1	1.5
Th	66.7	83.6	94.0	95.0
U	7.1	13.9	31.5	23.6
Si	88.4	91.7	94.8	92.1
Al	29.4	39.0	59.5	57.3
Fe	98.5	91.1	93.5	90.8
Mg	0.4	0.1	0.2	0.1
Ca	0.4	0.1	1.4	0.4
Na	4.9	3.7	4.5	3.4
K	0.9	0.4	1.5	0.5
Ti	98.1	99.1	99.5	99.6
P	89.8	89.9	92.8	89.3
Mn	1.1	1.1	1.2	1.1

Figure 3 - pH Profile Charts for MgO



SGS performed two additional tests, PN12 and PN14. Tests PN12 and PN14 were conducted using commercially available MgO products near Halleck Creek as a comparison to the locally available MgO used in the other tests.

Test PN13 reduced the residence time of primary neutralization from 2 hours to 1 hour. Reducing the residence time to one hour reduces equipment size and reduces REE losses to precipitation, which ultimately will increase overall rare earth oxide recoveries.

Table 3 – Comparison of Residence Time in Primary Neutralization

Primary Neutralization

Test ID	PN11	PN13
Feed	AL22 Filtrate	AL22 Filtrate
Reagent	MgO	MgO
Reagent Strength (% w/w)	15%	15%
pH Target	3.15	3.15
Retention Time (h)[1]	2	1
Temperature (°C)	75	75
Reagent Addition (kg/m^3)	24	28
Est. Filtration Rate (kg/m^2h)	1.7	0.8

[1] for each pH target, as applicable

* client supplied sample

Precipitation (%)[1]	PN11	PN13
LREE Avg	3.2	1.2
HREE Avg	3.2	2.1
Th	92.2	94.0
U	39.1	31.5
Si	94.6	94.8
Al	43.2	59.5
Fe	95.9	93.5
Mg	1.1	0.2
Ca	42.5	1.4
Na	6.2	4.5
K	2.6	1.5
Ti	98.9	99.5
P	92.7	92.8
Mn	1.4	1.2

[1] overall, potentially skewed by partial sampling

Secondary Neutralization (“SN”)

To remove the remaining iron, silica, aluminum, uranium and thorium from solution, SGS performed a pH profile test, SN1, for nominal pH ranges from 4.0, 4.5, 5.0, 5.5 and 6.0, see Table 5. Figure 4 below shows that nearly all the remaining iron, aluminum and thorium are precipitated at a pH near 5.0. Figure 4 also shows that Dy is starting to precipitate at pH 5.0.

Endpoint pH tests were conducted using pH values of 5.0 and 5.25, tests SN2 and SN3, respectively, see Table 5. Based on these two observations, SGS and the ARR team determined that secondary neutralization is best achieved at a target pH of 5.0.

A final leachate solution was prepared by using leachate from test PN11 using the parameters in test SN2. The resulting leach solution will be used for bench scale ion exchange removal of residual uranium and to feed into oxalic acid precipitation to produce a mixed rare earth oxalate. These tests will be completed prior to the end of the year.

Table 4 – Secondary Neutralization Tests

Secondary Neutralization

Test ID	SN1	SN2	SN3
Feed	PN11 Filtrate	PN11 Filtrate	PN11 Filtrate
Reagent	MgO	MgO	MgO
Reagent Strength (% w/w)	15%	5-10%	5-10%
pH Target	4 - 6	5.00	5.25
Retention Time (h)1	1	2	2
Temperature (°C)	75	75	75
Reagent Addition (kg/m3)	3	3	3
Est. Filtration Rate (kg/m2h)	4.8	5.1	5.8

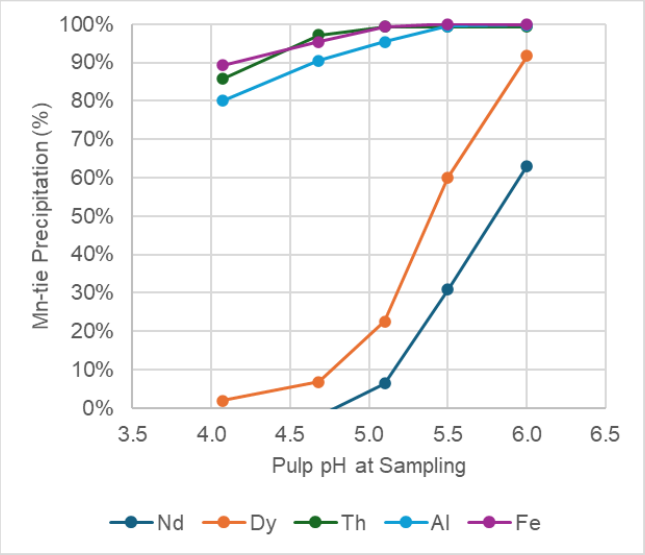
1 for each pH target, as applicable

* client supplied sample

Precipitation (%)[1]	SN1	SN2	SN3
LREE Avg	49.1	7.6	12.3
HREE Avg	81.9	16.7	28.5
Th	98.1	98.9	98.9
U	81.6	19.8	36.3
Si	95.2	71.0	72.6
Al	96.7	96.3	99.5
Fe	98.5	99.4	99.6
Mg	1.1	0.1	0.2
Ca	1.4	0.3	0.5
Na	1.2	0.6	0.6
K	0.4	0.1	0.1
Ti	99.4	95.6	97.1
P	14.4	10.4	11.6
Mn	2.9	0.3	0.7
Zn	-	-	-

1. Overall, potentially skewed by partial sampling

Figure 4 - pH Profile Charts for Secondary Neutralization



It should be noted, to prevent REE losses in the system, SGS and Tetra Tech recommend that the precipitated solids generated during secondary neutralization be recycled to the leach circuit andre-dissolved. While this increases the total volume of material being leached by about 1% or 2%, capturing the REE in this material is most beneficial for the project.

This release was authorised by the board of American Rare Earths.

Investors can follow the Company's progress at www.americanree.com

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Competent Person(s) Statement:

Competent Persons Statement: The information in this document is based on information compiled by personnel under the direction of Mr. Dwight Kinnes. This work was reviewed and approved for release by Mr. Dwight Kinnes (Society of Mining Engineers #4063295RM) who is employed by American Rare Earths and has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 JORC Code. Mr. Kinnes consents to the inclusion in the report of the matters based upon the information in the form and context in which it appears.

ARR confirms it is not aware of any new information or data that materially affects the information included in the original market announcement, and, in the case of estimates of Mineral Resources, that all material assumptions and technical parameters underpinning the estimates in the relevant market announcements continue to apply and have not materially changed. ARR confirms that the form and context in which the Competent Person's findings presented have not been materially modified from the original market announcement.

This work was reviewed and approved for release by Mr. Kelton Smith (Society of Mining Engineers #4227309RM) who is employed by Tetra Tech and has sufficient experience which is relevant to the processing, separation, metallurgical testing and type of deposit under consideration and to the activity which he is undertaking as a Competent Person as defined in the 2012 JORC Code. Mr. Smith is an experienced technical manager with a degree in Chemical engineering, operations management and engineering management. He has held several senior engineering management roles at rare earth companies (Molycorp and NioCorp) as well as ample rare earth experience as an industry consultant. Mr. Smith consents to the inclusion in the report of the matters based upon the information in the form and context in which it appears.

About American Rare Earths Limited:

American Rare Earths (ASX: ARR | OTCQX: ARRNF | ADR: AMRRY) is a critical minerals company at the forefront of reshaping the U.S. rare earths industry. Through its wholly owned subsidiary, Wyoming Rare (USA) Inc. ("WRI"), the company is advancing the Halleck Creek Project in Wyoming—a world-class rare earth deposit with the potential to secure America's critical mineral independence for generations. Located on Wyoming State land, the Cowboy State Mine within Halleck Creek offers cost-efficient open-pit mining methods and benefits from streamlined permitting processes in this mining-friendly state.

With plans for onsite mineral processing and separation facilities, Halleck Creek is strategically positioned to reduce U.S. reliance on imports—predominantly from China—while meeting the growing demand for rare earth elements essential to defense, advanced technologies, and economic security. As exploration progresses, the project's untapped potential on both State and Federal lands further reinforces its significance as a cornerstone of U.S. supply chain security. In addition to its resource potential, American Rare Earths is committed to environmentally responsible mining practices and continues to collaborate with U.S. Government-supported R&D programs to develop innovative extraction and processing technologies for rare earth elements.

Appendix A – Halleck Creek JORC Table 1

Section 1 Sampling Techniques and Data		
(Criteria in this section apply to all succeeding sections.)		
Criteria	***JORC Code explanation***	**Commentary**
Sampling techniques	*Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as downhole gamma sondes, handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.*	In 2024, WRI drilled 28 drill holes at the Cowboy State Mine area. This included 11 HQ-sized core holes (1,586 m total) and 17 reverse circulation (RC) holes (1,866 m total). RC chip samples were collected at 1.5 m intervals via rotary splitter, while core samples were collected every 3 m of at lithological contacts. ARR drilled 15 reverse circulation (RC) holes and eight HQ-sized diamond core holes between September and October 2023. All RC holes were 102 meters (334.65 feet) deep, with seven core holes at 80 meters (262.47 feet) and one deep core hole at 302 m (990.81 feet). RC chip samples were collected at a 1.5-meter (4.92 ft) continuous interval via rotary splitter. Rock core was divided into sample lengths of 1.5 m (4.92 feet) long and at key lithological breaks. ARR drilled 38 reverse circulation (RC) holes across the Halleck Creek Resource Claim area between October and December 2022. All holes were approximately 150 meters (492.13 feet) deep, with the exception of HC22-RM015 which went to a depth of 175.5 meters (576 feet). Chip samples were collected at 1.5-meter continuous intervals via rotary splitter.

Section 1 Sampling Techniques and Data		
(Criteria in this section apply to all succeeding sections.)		
Criteria	***JORC Code explanation***	**Commentary**
		In March and April 2022, ARR drilled nine HQ-sized core holes across the Halleck Creek Resource claim area. All holes were approximately 350 ft with the exception of one hole which was terminated at 194 ft. Total drilled length of 3,008 ft (917 m). Rock core was divided into sample lengths of 5 ft (1.52 m) long and at key lithological breaks. A total of 734 surface rock samples exist in the Halleck Creek database. Surface rock samples collected by ARR are logged, photographed and located using handheld GPS units. As part of reverse circulation (RC) and diamond core exploration drilling at Halleck Creek, ARR collected XRF readings on RC chip and core samples. Elements included in XRF measurements include Lanthanum, Cerium, Neodymium, and Praseodymium. ARR collected three XRF readings on each sample, then averaged the readings. Readings are performed at 20-meter intervals down each drill hole. These values are qualitative in nature and provide only rough indications of grade.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	Core and RC samples were processed and logged systematically. Quality control included inserting certified reference materials (CRMs), blanks, and duplicates into the sampling stream.
	Aspects of the determination of mineralisation that are Material to the Public Report.	The Red Mountain Pluton (RMP) of the Halleck Creek Rare Earths Project is a distinctly layered monzonitic to syenitic body which exhibits significant and widespread REE enrichment. Enrichment is

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	***JORC Code explanation***	**Commentary**
		dependent on allanite abundance, a sorosilicate of the epidote group. Allanite occurs in all three units of the RMP, the clinopyroxene quartz monzonite, the biotite-hornblende quartz syenite, and the fayalite monzonite, in variable abundances.
	In cases where 'industry standard' work has been done, this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	Reverse circulation rock chip samples were collected at 1.5-meter continuous intervals via rotary splitter. For each interval chip samples were placed in labelled sample bags weighing between 1-2kg. A 0.5-1kg sample was collected for reserve analysis and logging. Chip samples were also placed into chip trays with 20 slots for logging and XRF analysis. Rock core samples 5 ft (1.52 m) long are fillet cut. The fillet cuts are being pulverised and sampled for 60 elements including rare earth elements using ICP-MS and industry standards. A select number of samples are additionally being assayed for whole rock geochemistry. RC chip samples were sent to ALS labs in Twin Falls, ID for preparation and forwarded on to ALS labs in Vancouver, BC for ICP-MS analysis. ALS analysis: ME-MS81. Core samples were first sent to ALS in Reno, NV, for cutting and preparation, and also sent to Vancouver, BC for the same suite of testwork.

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	***JORC Code explanation***	**Commentary**
		ALS Laboratories in BC, Canada has performed detailed assay analysis for the project since the fall of 2022. American Assay Labs in Sparks, NV is performed the analyses for the Spring 2022 program.
Drilling techniques	*Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or another type, whether the core is oriented and if so, by what method, etc.).*	Drilling included HQ diamond drilling for core samples using a Marcotte HTM 2500 rig and rotary split RC drilling with a Schramm T455-GT rig. Oriented core was collected where applicable to support structural analysis.
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed.*	A continuous rotary sample splitter was used to collect the RC samples at 1.5m intervals. All drill core was visually logged, measured, and photographed by ARR geologists. Drill core was collected in lengths (runs) of 1.5m (~5 ft). Recoveries were calculated for each core run.
	Measures are taken to maximise sample recovery and ensure the representative nature of the samples.	Reverse circulation rock chip samples were collected at 1.5-meter continuous intervals via rotary splitter. For each interval chip samples were placed in labelled sample bags weighing between 1-2kg. A 0.5-1kg sample was collected for reserve analysis and logging. Chip samples were also placed into chip trays with 20 slots for logging and XRF analysis.

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
		All core and associated samples were immediately placed in core boxes. In 2024, acoustic televiewer surveys provided supplementary data on structural continuity. Natural gamma logs were also collected for each 2024 drill hole which correlate with TREO grades.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	Recoveries were very high in competent rock. No loss or gain of grade or grade bias related to recovery
Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	All RC samples were visually logged by ARR geologists from chip trays using 10x binocular microscopes. Samples at 25m intervals were photos and analysed using an Olympus Vanta handheld XRF analyser in triplicate. Lanthanum, Cerium, Neodymium, and Praseodymium were analysed via XRF. All drill core was visually logged, measured, and photographed by ARR geologists. Drill core was collected in lengths (runs) of 1.5 meters (~5 ft). ARR geologists calculated recoveries for each core run. ARR geologists logged lithology, various types of alteration and mineralisation, fractures, fracture conditions, and RQD. Alpha and beta fracture angles were determined from oriented core in 2024.

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	*JORC Code explanation*	**Commentary**
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	RC samples and logging is quantitative in nature. Chip samples are stored in secure sample trays. Chip samples were photographed and 25m intervals. Core logging is quantitative in nature. All core was photographed wet and dry.
	The total length and percentage of the relevant intersections logged.	All RC samples were visually logged by ARR geologists for each 1.5-meter continuous sample. All drill core was visually logged, measured, and photographed by ARR geologists. Drill core was collected in lengths (runs) of 5 feet (1.52m). ARR geologists calculated recoveries for each core run. ARR geologists logged lithology, various types of alteration and mineralisation, fractures, fracture conditions, and RQD.
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.*	RC chip samples were not cut. Drill core was fillet cut by ALS Laboratories with approximately 1/2 of the core used for assay. The remaining core material will be kept in reserve by ALS until sent for future metallurgical testwork.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	Samples varied between wet and dry. The course crystalline nature of the deposit minimizes adverse effects of wet samples. Samples were rotary split during drilling and sample collection. ALS labs dried wet samples using their DRY-21 drying process.

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	***JORC Code explanation***	**Commentary**
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	RC samples were taken from pulverize splits of up to 250 g to better than 85 % passing minus 75 microns. All core samples were dry. Sample preparation: 1kg samples split to 250g for pulverising to -75 microns. Sample analysis: 0.5g charge assayed by ICP-MS technique. Both sampling methods are considered appropriate for the type of material collected and are considered industry standard.
	Quality control procedures adopted for all sub-sampling stages to maximise the representivity of samples.	ARR submitted CRM sample blanks, CRM standard REE samples from CND Labs and duplicate samples for analysis. Each CRM blank, REE standard, and duplicate were rotated into both the RC and core sampling process every 20 samples.
	Measures are taken to ensure that the sampling is representative of the in situ material collected, including, for instance, results for field duplicate/second-half sampling.	RC samples were collected using a continuous feed rotary split sampler. Fillet cuts along the entire length of all core are representative of the in-situ material.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Allanite is generally well distributed across the core and the sample sizes are representative of the fine grain size of the Allanite.

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	***JORC Code explanation***	**Commentary**
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	ALS uses a 5-acid digestion and 32 elements by lithium borate fusion and ICP-MS (ME-MS81). For quantitative results of all elements, including those encapsulated in resistive minerals. These assays include all rare earth elements. AAL Labs uses 5-acid digestion and 48 element analysis including REE reported in ppm using method REE-5AO48 and whole-rock geochemical XRF analysis using method X-LIB15.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	Samples at 25m intervals were photographed and analysed using an Olympus Vanta handheld XRF analyser in triplicate. Lanthanum, Cerium, Neodymium, and Praseodymium were analysed. Simple average values of three XRF readings were calculated. Seven of the core holes received ATV/OTV logging as well as slim hole induction which recorded natural gamma and conductivity/resistivity. Geophysical logging was completed by Century Geophysical located in Gillette, WY in 2023. DGI Geosciences, Salt Lake City, UT, performed logging in 2024. All tools were properly calibrated prior to logging.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	For the 2024 drilling program, ARR submitted CRM sample blanks, CRM standard REE samples from CDN Labs, and duplicate samples for analysis. QA/QC samples, including CRM and blank samples, were inserted alternately at every 20th sample for both RC and core

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	*JORC Code explanation*	Commentary
		drilling. ALS Laboratories also incorporated their own QA/QC procedures to ensure analytical reliability. For the RC drilling, ARR submitted CRM sample blanks, CRM standard REE samples from CND Labs and duplicate samples for analysis. CRM and Blank samples were inserted alternately at 20 sample intervals. The same was done for the core drilling completed Fall 2023. ALS Laboratories additionally incorporated their own Qa/Qc procedure. For core drilling completed Spring 2022, ARR submitted CRM sample blanks, CRM standard REE samples from CND Labs and duplicate samples for analysis. Blank samples were added one for every 10 core samples, REE samples were added one for every 25 core samples, and Duplicate samples were added one per every 25 core samples. Internal laboratory blanks and standards will additionally be inserted during analysis.
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.*	RC chip samples have not yet been verified by independent personnel. Consulting company personnel have observed the assayed core samples. Company personnel sampled the entire length of each hole.
	The use of twinned holes.	No twinned holes were used.

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	***JORC Code explanation***	**Commentary**
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Data entry was performed by ARR personnel and checked by ARR geologists. All field logs were scanned and uploaded to company file servers. All photographs of the core were also uploaded to the file server daily. Drilling data will be imported into the DHDB drill hole database. All scanned documents are cross-referenced and directly available from the database. Assay data from the RC samples was imported into the database directly from electronic spreadsheets sent to ARR from ALS. Core assay data was received electronically from AAL labs. These raw data as elements reported ppm were imported into the database with no adjustments.
	Discuss any adjustment to assay data.	Assay data is stored in the database in elemental form. Reporting of oxide values are calculated in the database using the molar mass of the element and the oxide.
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*	All drill hole collars were surveyed by a registered professional land surveyor. Deviation surveys were conducted post-drilling to confirm subsurface data accuracy.
	Specification of the grid system used.	The grid system used to compile data was NAD83 Zone 13N.
	Quality and adequacy of topographic control.	Topography control is +/- 10 ft (3 m).

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	***JORC Code explanation***	**Commentary**
Data spacing and distribution	*Data spacing for reporting of Exploration Results.*	Drill spacing varied between 100 and 300 m, with infill drilling conducted to refine the resource model and improve classification confidence.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	Spacing supports classification into Indicated and Inferred categories based on geostatistical analysis and grade continuity confirmed through cross-sections and swath plots.
	Whether sample compositing has been applied.	Sample compositing was applied during resource estimation. Grade intervals were composited to 1.5 m (5 feet), the dominant sampling interval, ensuring compatibility with the data collected and supporting accurate resource estimation.
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	Mineralization at Halleck Creek is a function of fractional crystallization of allanite in syenitic rocks of the Red Mountain Pluton. Mineralization is not structurally controlled and exploration drilling to date does not reveal any preferential mineralization related to geologic structures. Therefore, orientation of drilling does not bias sampling.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	Orientation of drilling does not bias sampling.
Sample security	*The measures are taken to ensure sample security.*	All RC chip samples were collected from the drill rigs and stored in a secured and locked facility. Sample pallets were shipped weekly,

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	***JORC Code explanation***	**Commentary**
		by bonded carrier, directly to ALS labs in Twin Falls, ID. Chains of custody were maintained at all times. All core was collected from the drill rig daily and stored in a secure, locked facility until the core was dispatched by bonded courier to ALS Laboratories. Chains of custody were maintained at all times. All rock samples were in the direct control of company geologists until dispatched to American Assay Labs.
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	No external audits or reviews have been conducted to date. However, sampling techniques are consistent with industry standards.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership, including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*	ARR controls 364 unpatented federal lode claims and 4 Wyoming State mineral licenses covering 3,280 ha (8,108 acres).
	The security of the tenure held at the time of reporting and any known impediments to obtaining a licence to operate in the area.	No impediments to holding the claims exist. To maintain the claims an annual holding fee of $165/claim is payable to the BLM. To maintain the State leases minimum rental payments of $1/acre for 1-5 years; $2/acre for 6-10 years; and $3/acre if held for 10 years or longer.
Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	Prior to sampling by WIM on behalf of Blackfire Minerals and Zenith there was no previous sampling by any other groups within the ARR claim and Wyoming State Lease blocks.
Geology	*Deposit type, geological setting and style of mineralisation.*	The REE's occur within Allanite which occurs as a variable constituent of the Red Mountain Pluton. The occurrence can be characterised as a disseminated rare earth deposit.
Drill hole Information	*A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:*	For the 2023 and 2024 exploration programs, FTE DRILLING USA INC. of Mount Uniacke, Nova Scotia used a Schraam T-450 track mounted rig to drill 15 reverse circulation drill holes. Drill hole depths for 37 holes was 102 m. FTE also utilized an enclosed Versa-Drilling diamond core rig to drill eight HQ-sized core holes.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
		For the Fall 2022 program, FTE DRILLING USA INC. of Mount Uniacke, Nova Scotia used a Schraam T-450 track mounted rig to drill 37 reverse circulation drill holes. Drill hole depths for 37 holes was 150m and one hole at 175.5m Authentic Drilling from Kiowa, Colorado used both a track mounted and ATV mounted core rig to drill nine HQ diameter core holes. From March to April 2022, ARR drilled nine core holes across the Halleck Creek claim area. Drill holes ranged in depth from 194 to 352.5 ft with a total drilled length of 3,008 ft (917 m).
	easting and northing of the drill hole collar	Drilling information from the 2024 exploration program was published in the report "Technical Report of Exploration and Updated Resource Estimates at Red Mountain of the Halleck Creek Rare Earths Project", December 2024. Drilling information from the Fall 2023 campaign was published in the report "Summary of 2023 Infill Drilling at the Halleck Creek Project Area", November 2023 Drilling information from the Fall 2022 drilling campaign is presented in detail in the "Technical Report of Exploration and Maiden Resource Estimates of the Halleck Creek Rare Earths Project", March 2023.
	elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar	
	dip and azimuth of the hole	
	downhole length and interception depth	
	Hole length.	

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	No Drilling data has been excluded.
Data aggregation methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.*	Average Grade values were cut at minimum of TREO 1,000 ppm.
	Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Assays are representative of each 1.50 m, (~5 ft) sample interval.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalents used.
Relationship between mineralisation widths and intercept lengths	*These relationships are particularly important in the reporting of Exploration Results.* *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.*	Allanite mineralization observed at Halleck Creek occurs uniformly throughout the CQM and BHS rocks of within the Red Mountain Pluton. Therefore, the geometry of mineralisation does not vary with drill hole orientation or angle within homogeneous rock types.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	*JORC Code explanation*	Commentary
	If it is unknown and only the downhole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	
Diagrams	*Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to, a plan view of drill hole collar locations and appropriate sectional views.*	Location information is presented in detail in the "Technical Report of Exploration and Updated Resource Estimates at Red Mountain of the Halleck Creek Rare Earths Project", December 2024.
Balanced reporting	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practised to avoid misleading reporting of Exploration Results.*	Reporting of the most recent exploration data is included in the "Technical Report of Exploration and Updated Resource Estimates at Red Mountain of the Halleck Creek Rare Earths Project", December 2024. Previous data is presented in the "Technical Report of Exploration and Maiden Resource Estimates of the Halleck Creek Rare Earths Project", March 2023, and in report "Summary of 2023 Infill Drilling at the Halleck Creek Project Area", November 2023.
Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported, including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test*	In hand specimen this rock is a red colored, hard and dense granite with areas of localized fracturing. The rock shows significant iron staining and deep weathering.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
	results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	Microscopic description: In hand specimen the samples represent light colored, fairly coarse-grained granitic rock composed of visible secondary iron oxide, amphibole, opaques, clear quartz and pink to white colored feldspar. All of the specimens show moderate to strong weathering and fracturing. Allanite content is variable from trace to 2%. Rare Earths are found within the Allanite. Historical metallurgical testing consisted of concentrating the Allanite by both gravity and magnetic separation. The current program employs sequential gravity separation and magnetic separation to produce a concentrate suitable for downstream rare earth elements extraction.
Further work	*The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).*	Detailed geological mapping and channel sampling is planned to enhance further development drilling to increase confidence levels of resources.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Geological mapping and channel sampling is planned for the Bluegrass and County Line project areas to potentially expand mineral resources beyond the Cowboy State Mine area.

Section 3 Estimation and Reporting of Mineral Resources		
(Criteria listed in the preceding section also apply to this section.)		
Criteria	***JORC Code explanation***	**Commentary**
Database integrity	*Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* *Data validation procedures used.*	Drill hole data header, lithologic data checked by field geologists and by visual examination on maps and drill hole striplogs. Assay and Qa/Qc data were imported into the database directly from electronic spreadsheets provide by laboratories. Histograms graphical logs were also prepared and reviewed by ARR geologists.
Site visits	*Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* *If no site visits have been undertaken indicate why this is the case.*	Mr. Dwight Kinnes visited the Halleck Creek site numerous times in 2024 and 2025. Mr. Patrick Sobecke and Mr. Erick Kennedy of Stantec visited the site on February 10, 2025. Mr. Alf Gillman of Odessa Resources and Mr. Kelton Smith of Tetra Tech visited the site on March 7, 2024.
Geological interpretation	*Confidence in (or conversely, the uncertainty of) the geological*	The Halleck Creek RE deposit is contained with rocks of the Red Mountain Pluton. These rocks consist primarily of clinopyroxene quartz monzonite (CQM), and biotite hornblende syenite (BHS). These two lithologies are difficult to visually distinguish. However, the concentration of rare earth elements is observable between lithologies.

Section 3 Estimation and Reporting of Mineral Resources		
(Criteria listed in the preceding section also apply to this section.)		
Criteria	***JORC Code explanation***	**Commentary**
	interpretation of the mineral deposit. *Nature of the data used and of any assumptions made.* *The effect, if any, of alternative interpretations on Mineral Resource estimation.* *The use of geology in guiding and controlling Mineral Resource estimation.* *The factors affecting continuity both of grade and geology.*	Rocks of the Elmers Rock Greenstone Belt (ERGB) and the Sybille (Syb) intrusion are easily distinguishable from rocks of the RMP. These rock units are essentially barren of rare earth elements. Therefore, the confidence in discerning rocks of the RMP from is high. The extent of the RMP relative to other units was outlined into modelling domains used for resource estimates. The distribution of allanite throughout CQM and BHS rocks of the RMP is generally uniform and is not structurally controlled. Potassic alternation observed does not appear to affect the grade of allanite throughout the deposit.
Dimensions	*The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower*	The Halleck Creek REE project currently contains two primary resource areas: the Red Mountain area and the Overton Mountain area. Resources also extend into the Bluegrass resource area. The Cowboy State Mine area is a subset of Red Mountain cover land minerals owned by the state of Wyoming, and under lease by WRI. The Red Mountain resource area is bounded to the west by the ERGB, and to the south by the Syb. Archean granites bound the Red Mountain area to the east.

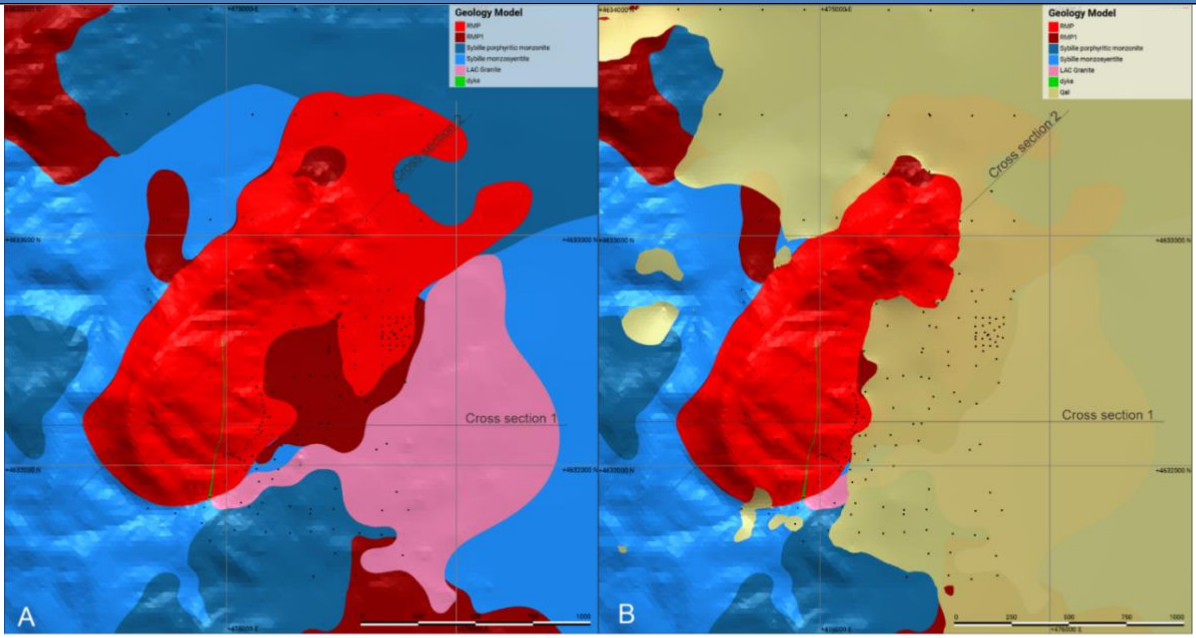
Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
	limits of the Mineral Resource.	RC samples with TREO grades exceeding 1,500 ppm occurred at the base of 37 drill holes in the Red Mountain resource area extending down to depths of 150m with one hole extending to a depth of 175.5m. Therefore, ARR considers the Red Mountain resource area to be open at depth. The Overton Mountain resource area is bounded to the west by mineral claims, and therefore, remains open to the west. Lower grade BHS rocks occur at the northern end of Overton Mountain. Drilling data to the east and south indicate that the Overton Mountain resource area remains open across Bluegrass Creek. Like the Red Mountain drilling, RC samples at Overton Mountain contained TREO assay values exceeding 3,500 ppm to depths of 150m in 18 holes. One, 302m diamond core hole additionally exhibited grades exceeding 2,000 ppm to the bottom of the hole. Therefore, ARR considers the Overton Mountain resource area to be open at depth.
Estimation and modelling techniques	*The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of*	A revised three-dimensional geological model was developed Odessa Resources Pty. Ltd., from Perth Australia, using both drillhole information and surface mapping to isolate the higher-grade RMP domain from the surrounding lithologies. The domains that are modelled comprise the primary geological units as interpreted by ARR geologists. These geological domains consist of: • QAL Quaternary alluvium • RMP Red Mountain Pluton comprising mostly clinopyroxene quartz monzonite (CQM) • RMP1 comprising mostly biotite-hornblende quartz syenite and fayalite monzonite • ERGB unmineralized Elmers Rock Greenstone Belt • SYB low grade monzonite Sybille intrusions • LAC Laramie Anorthosite Complex Geochemical surface sample results were incorporated into the model but only to define the outer limits of the resource block domains. The Figures below show the general arrangement of the geological domains.

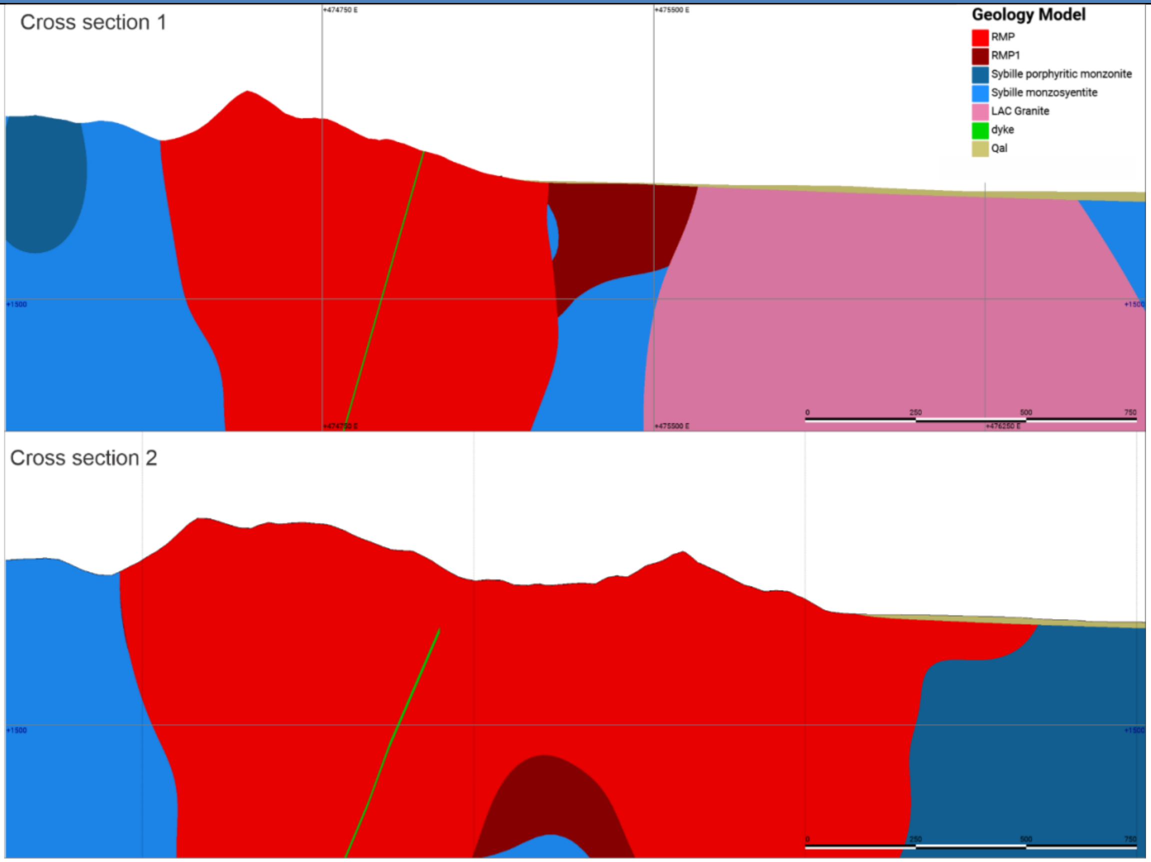
Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
	computer software and parameters used. *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* *The assumptions made regarding recovery of by-products.* *Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).* *In the case of block model interpolation, the block size in*	

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
	relation to the average sample spacing and the search employed. *Any assumptions behind modelling of selective mining units.* *Any assumptions about correlation between variables.* *Description of how the geological interpretation was used to control the resource estimates.* *Discussion of basis for using or not using grade cutting or capping.* *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of*	 Odessa updated the Red Mountain resource model using Leapfrog Edge, with all drill hole data variograms and block model parameters were updated. Grade estimation was carried using an ordinary kriged ("OK") interpolant.

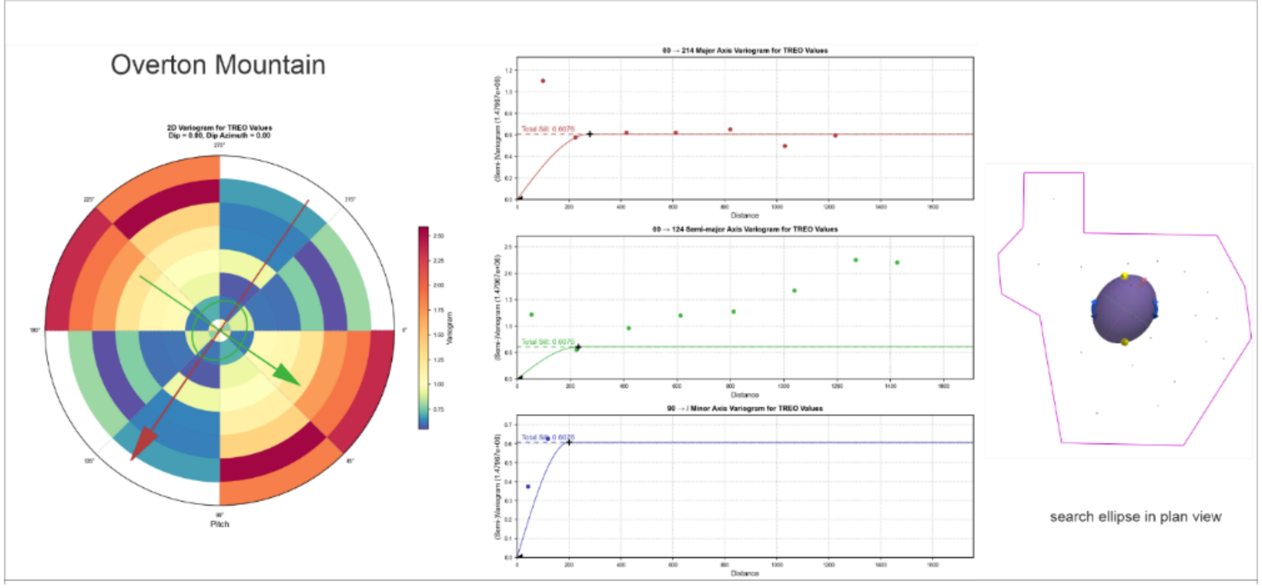
Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td>reconciliation data if available.</td><td>
Block Model Parameters
<table>
<tr><th>Block Model Parameter</th><th>Value</th></tr>
<tr><td>Parent Block Size</td><td>20m</td></tr>
<tr><td>Sub-block count (i, j, k)</td><td>4, 4, 4</td></tr>
<tr><td>Minimum block size (i, j, k)</td><td>5m ,5m, 2.5m</td></tr>
<tr><td>Base point (x, y, z)</td><td>473900.00, 4631300.00, 2000.00</td></tr>
<tr><td>Boundary size (W x L x H)</td><td>2060.00, 2040.00, 510.00</td></tr>
<tr><td>Azimuth</td><td>0</td></tr>
<tr><td>Dip</td><td>0</td></tr>
<tr><td>Pitch</td><td>0</td></tr>
<tr><td>Size in Blocks</td><td>103x102x51=535,806</td></tr>
</table>
<p>The block model contains attributes pertaining to resource block, resource category, grade class, geologic domain, and numerical attributes for TREO, rare earth oxides of all rare earth elements.</p>
<p>Geological domains focused on higher grade RMP and RMP1 lithologies which provided control of resource block boundaries along with variography.</p>
<table>
<tr><th>General</th><th colspan="3">Direction</th><th colspan="6">Structure 1</th></tr>
<tr><th>Variogram Name</th><th>Dip</th><th>Dip Azimuth</th><th>Pitch</th><th>Normalized Nugget</th><th>Normalized sill</th><th>Structure</th><th>Major</th><th>Semi-major</th><th>Minor</th></tr>
<tr><td>OM</td><td>0</td><td>0</td><td>124</td><td>0</td><td>0.6</td><td>Spherical</td><td>280</td><td>230</td><td>200</td></tr>
<tr><td>RM</td><td>0</td><td>0</td><td>90</td><td>0.1</td><td>0.8</td><td>Spherical</td><td>445</td><td>240</td><td>170</td></tr>
</table>
</td></tr>
</table>

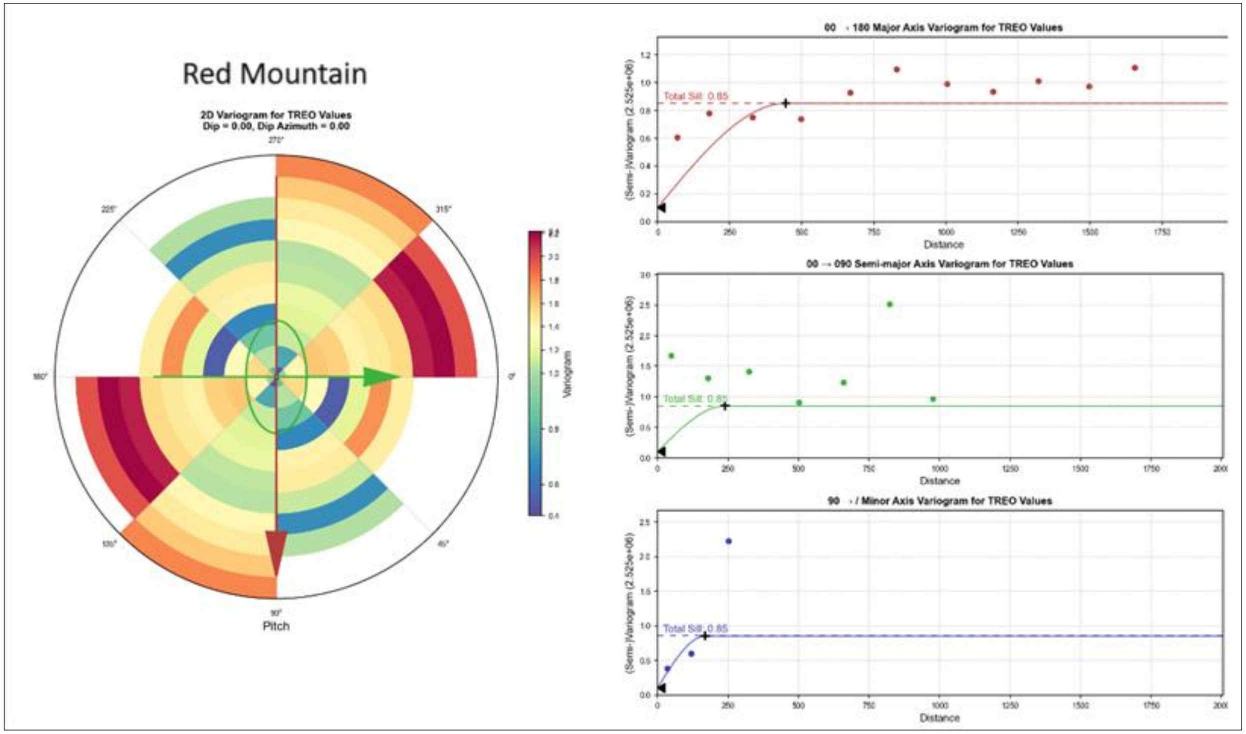
Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

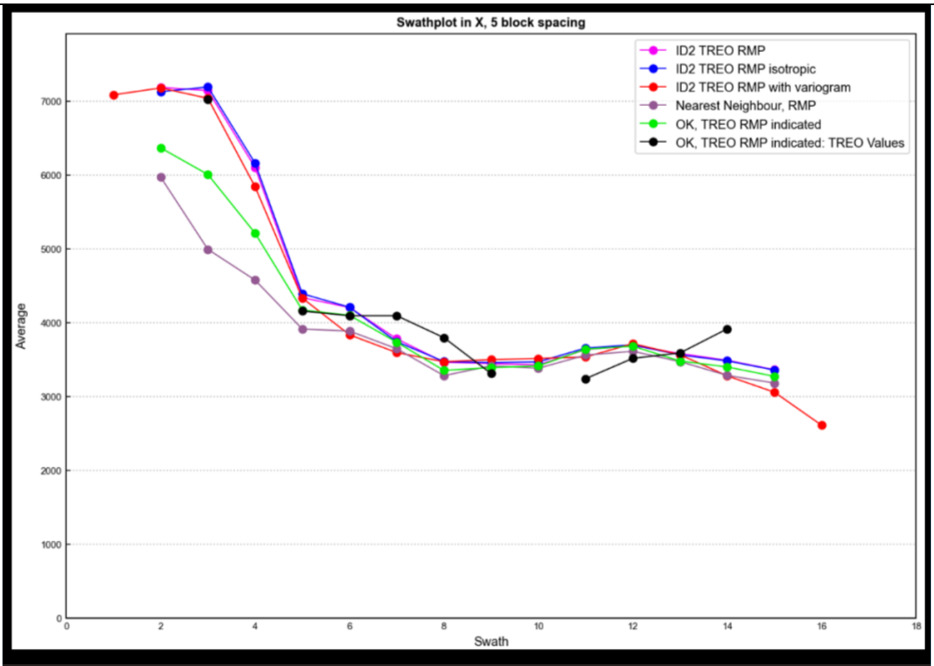
Criteria	***JORC Code explanation***	**Commentary**
		

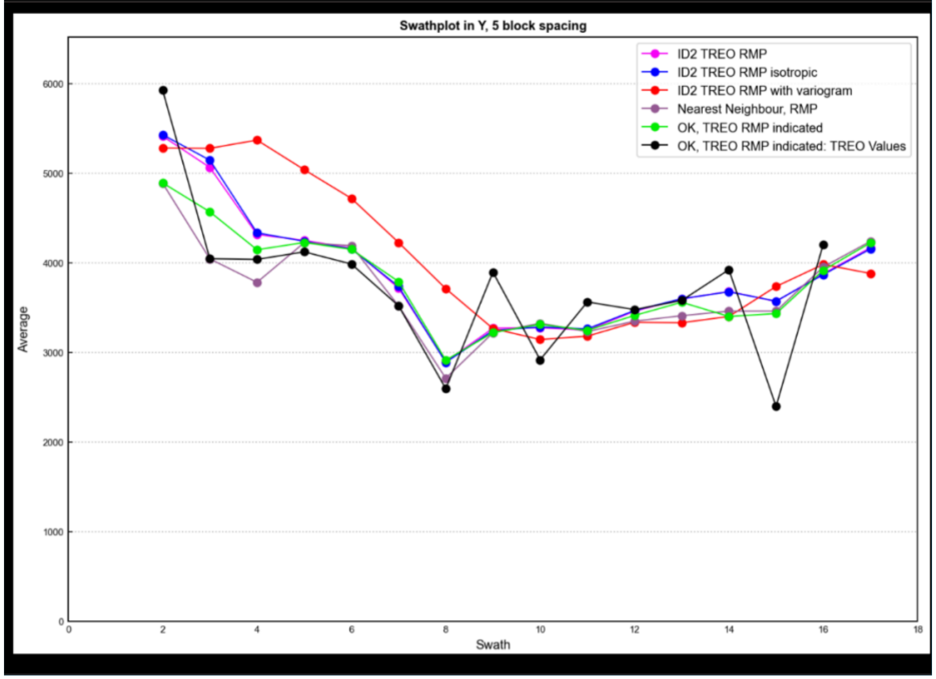
Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
		 Several estimation runs were carried out on the RMP Indicated resource to check for any variance between estimated grades and the input data. Modelled estimator: OK TREO RMP: Indicated ordinary kriged estimate with variogram model (150x150x120m search) The additional estimators:

Section 3 Estimation and Reporting of Mineral Resources		
(Criteria listed in the preceding section also apply to this section.)		
Criteria	***JORC Code explanation***	**Commentary**
		ID2 TREO RMP: Inverse Distance Squared (ID2) using horizontal plane (150x150x120m search) ID2 TREO RMP: isotropic Inverse Distance Squared (ID2) using an iso-tropic 150m search ellipse ID2 TREO RMP: with variogram Inverse Distance Squared (ID2) using the same estimation and variogram parameters as the kriged model (445x240x170m search) Nearest Neighbour, RMP: nearest neighbour estimate (150x150x120m search) These validation runs, together with the kriged estimator, were compared against the raw composite data in east-west (X) and north-south (Y) swath plots across the Red Mountain area (see below). The data indicate that the kriged estimator has done a reasonable job in estimating a global resource grade with no systematic bias towards overestimating the grades. The smoothing effects of the kriging interpolant is consistent with both the inherent nature of the kriging process and the large search ellipses used.


Swathplot in X, 5 block spacing
ID2 TREO RMP
ID2 TREO RMP isotropic
ID2 TREO RMP with variogram
Nearest Neighbour, RMP
OK, TREO RMP indicated
OK, TREO RMP indicated: TREO Values
Average
7000
6000
5000
4000
3000
2000
1000
0
0
2
4
6
8
10
12
14
16
18
Swath


Swathplot in Y, 5 block spacing
ID2 TREO RMP
ID2 TREO RMP isotropic
ID2 TREO RMP with variogram
Nearest Neighbour, RMP
OK, TREO RMP indicated
OK, TREO RMP indicated: TREO Values
Average
6000
5000
4000
3000
2000
1000
0
0
2
4
6
8
10
12
14
16
18
Swath

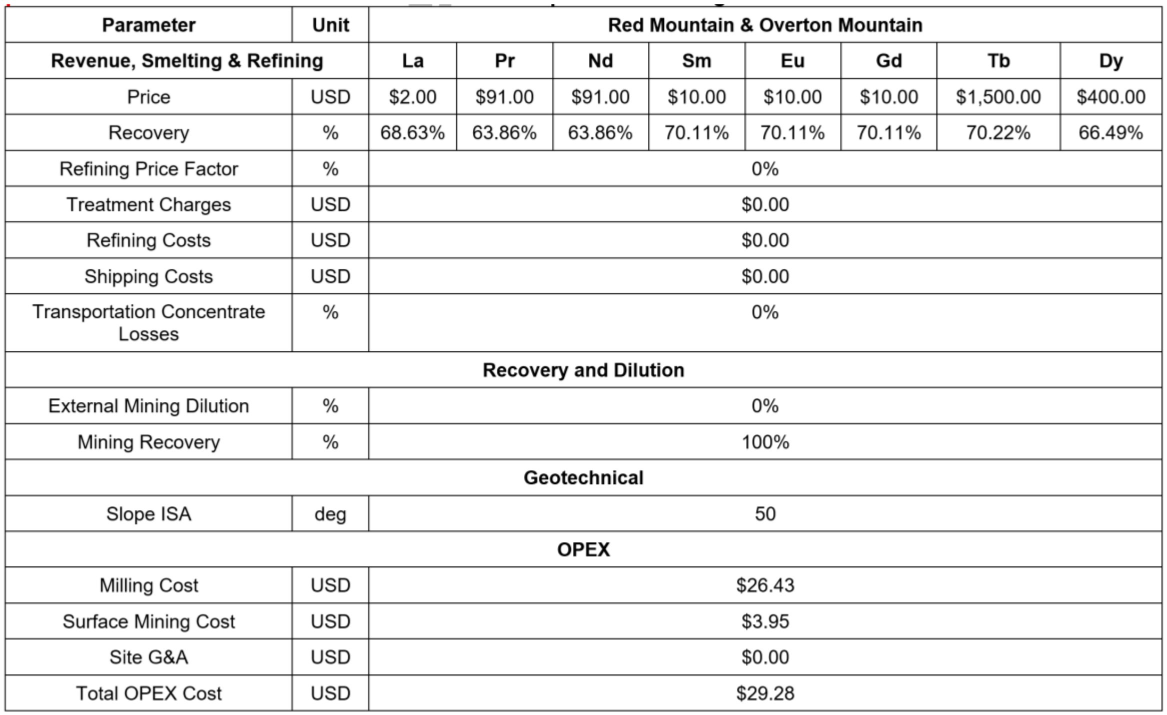
Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
Moisture	*Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	Tonnages are based on in-situ, dry basis.
Cut-off parameters	*The basis of the adopted cut-off grade(s) or quality parameters applied.*	A cut-off grade of 1,000 ppm TREO was applied to reported resource estimates based on preliminary net smelter calculations performed by Stantec.
Mining factors or assumptions	*Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but*	Surface mining was chosen as the method to extract the resource due to mineralization outcropping on surface and the homogeneity of the mineral grade over a large extent. In the absence of geotechnical data Stantec used reasonable bench angles, catch bench widths based on industry experience. Mining and metallurgical costs were from Stantec and Tetratech's respective cost databases for a mine and mill of this size and scale. Process recoveries were based on preliminary test work on samples of the mineralization. Mine design work was based on Geovia's Whittle mine software package, using a block model supplied by ARR and reviewed by Stantec for adequacy at a scoping level of study. The following mine design parameters were used in the pit design: Height between catch benches 6 m Bench Face Angle 70° Berm Width 2.9 m Total Road Allowance 18.5 m

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td>the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</td><td>
Maximum Ramp Grade 10%
Minimum Operating Width 30 m

<table>
<tr><th>Parameter</th><th>Unit</th><th colspan="8">Red Mountain & Overton Mountain</th></tr>
<tr><th colspan="2">Revenue, Smelting & Refining</th><th>La</th><th>Pr</th><th>Nd</th><th>Sm</th><th>Eu</th><th>Gd</th><th>Tb</th><th>Dy</th></tr>
<tr><td>Price</td><td>USD</td><td>$2.00</td><td>$91.00</td><td>$91.00</td><td>$10.00</td><td>$10.00</td><td>$10.00</td><td>$1,500.00</td><td>$400.00</td></tr>
<tr><td>Recovery</td><td>%</td><td>68.63%</td><td>63.86%</td><td>63.86%</td><td>70.11%</td><td>70.11%</td><td>70.11%</td><td>70.22%</td><td>66.49%</td></tr>
<tr><td>Refining Price Factor</td><td>%</td><td colspan="8">0%</td></tr>
<tr><td>Treatment Charges</td><td>USD</td><td colspan="8">$0.00</td></tr>
<tr><td>Refining Costs</td><td>USD</td><td colspan="8">$0.00</td></tr>
<tr><td>Shipping Costs</td><td>USD</td><td colspan="8">$0.00</td></tr>
<tr><td>Transportation Concentrate Losses</td><td>%</td><td colspan="8">0%</td></tr>
<tr><th colspan="10">Recovery and Dilution</th></tr>
<tr><td>External Mining Dilution</td><td>%</td><td colspan="8">0%</td></tr>
<tr><td>Mining Recovery</td><td>%</td><td colspan="8">100%</td></tr>
<tr><th colspan="10">Geotechnical</th></tr>
<tr><td>Slope ISA</td><td>deg</td><td colspan="8">50</td></tr>
<tr><th colspan="10">OPEX</th></tr>
<tr><td>Milling Cost</td><td>USD</td><td colspan="8">$26.43</td></tr>
<tr><td>Surface Mining Cost</td><td>USD</td><td colspan="8">$3.95</td></tr>
<tr><td>Site G&A</td><td>USD</td><td colspan="8">$0.00</td></tr>
<tr><td>Total OPEX Cost</td><td>USD</td><td colspan="8">$29.28</td></tr>
</table>
*OPEX costs are from 2023
</td></tr>
</table>

Section 3 Estimation and Reporting of Mineral Resources

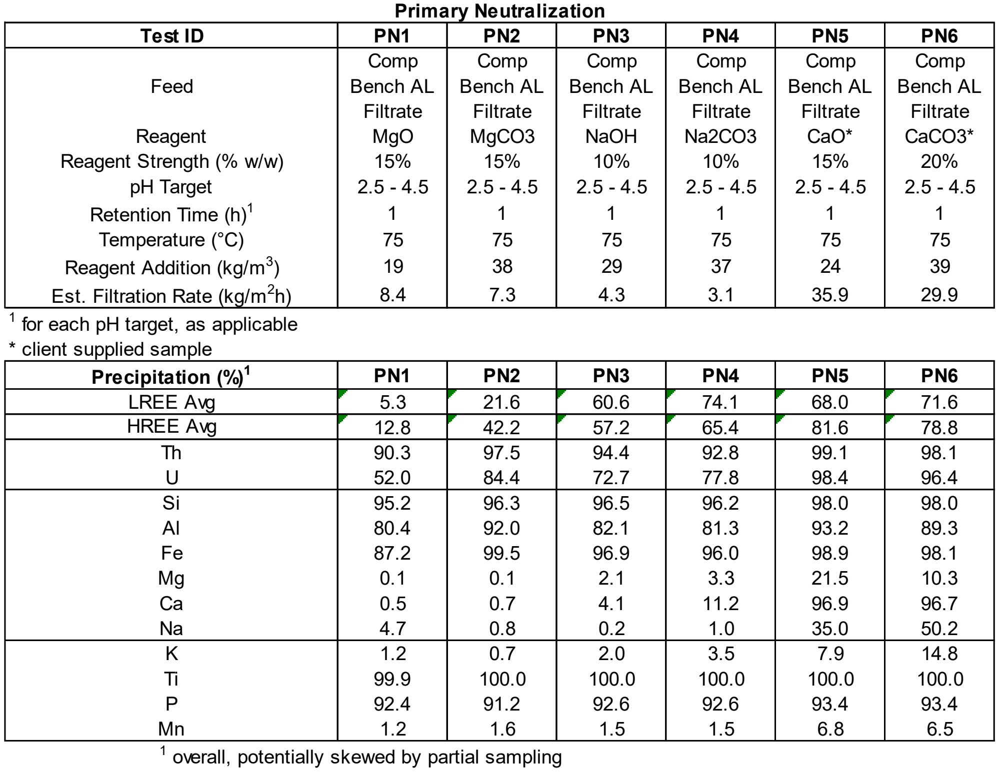
(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
		No mining dilution was used in the mine design of this study and a mining recovery of 100 % was assumed. Based on the chosen mining equipment, a minimum mining width of 30 meters was utilized. Measured, indicated and inferred mineral resources were included in the mine design, which is appropriate at a scoping level of study. Due to the homogeneity of the mineralization, while it is not reasonable to state that all inferred resources will be converted to a more precise mineral resource category, in general it is felt that it is reasonable to assume that the majority of the inferred resource will be converted to indicated or measured with additional sampling due to the size and homogeneity of the mineralized zone. Supporting mine infrastructure is discussed in the appropriate section of this report.
Metallurgical factors or assumptions	*The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting*	Impurity removal testing performed for the Halleck Creek Rare Earths project used leachate solutions prepared by SGS. ARR released the details of the sample material and the leach testing in the release date July 16, 2025. The leaching process successfully solubilizes the REE's but also leaches other elements that are present in the ore such as iron, aluminum, thorium and uranium. These elements must be removed from the leachate stream to ensure they do not carry through and deport to the product streams. The leachate also contains excess sulfuric acid, known as free acidity or terminal acidity, due to excess sulfuric acid being added in the leaching operation which is necessary to maximize recovery and kinetics. The free acidity must be neutralized using a base. Increasing the pH also results in precipitation of the impurity elements. **Primary Neutralization**The Primary Neutralization (Fe/Th Removal) consists of adding neutralizing agents to bring the leachate from ~30 g/L free acid to a pH of approximately 3.15. Neutralization of the leachate is required to remove free acidity left over from the leaching operation and to remove Fe/Th through a precipitation reaction at a higher pH. Hydrogen peroxide is added to increase the ORP value to ~600mV to oxidize iron from ferrous (Fe^{2+}) to ferric (Fe^{3+}) to drive precipitation of iron at a pH of 3.15. The 50% peroxide will be added as a volumetric ratio in cascade control from the ORP in the leachate. For the purposes of the mass balance and estimated peroxide usage a ratio of 0.53% v/v for 50% peroxide has been used based on laboratory testing.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
	Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.	Primary Neutralization tables below



Primary Neutralization

Test ID	**PN1**	**PN2**	**PN3**	**PN4**	**PN5**	**PN6**
Feed	Comp Bench AL Filtrate	Comp Bench AL Filtrate	Comp Bench AL Filtrate	Comp Bench AL Filtrate	Comp Bench AL Filtrate	Comp Bench AL Filtrate
Reagent	MgO	MgCO3	NaOH	Na2CO3	CaO*	CaCO3*
Reagent Strength (% w/w)	15%	15%	10%	10%	15%	20%
pH Target	2.5 - 4.5	2.5 - 4.5	2.5 - 4.5	2.5 - 4.5	2.5 - 4.5	2.5 - 4.5
Retention Time (h)[1]	1	1	1	1	1	1
Temperature (°C)	75	75	75	75	75	75
Reagent Addition (kg/m^3)	19	38	29	37	24	39
Est. Filtration Rate (kg/m^2h)	8.4	7.3	4.3	3.1	35.9	29.9

[1] for each pH target, as applicable

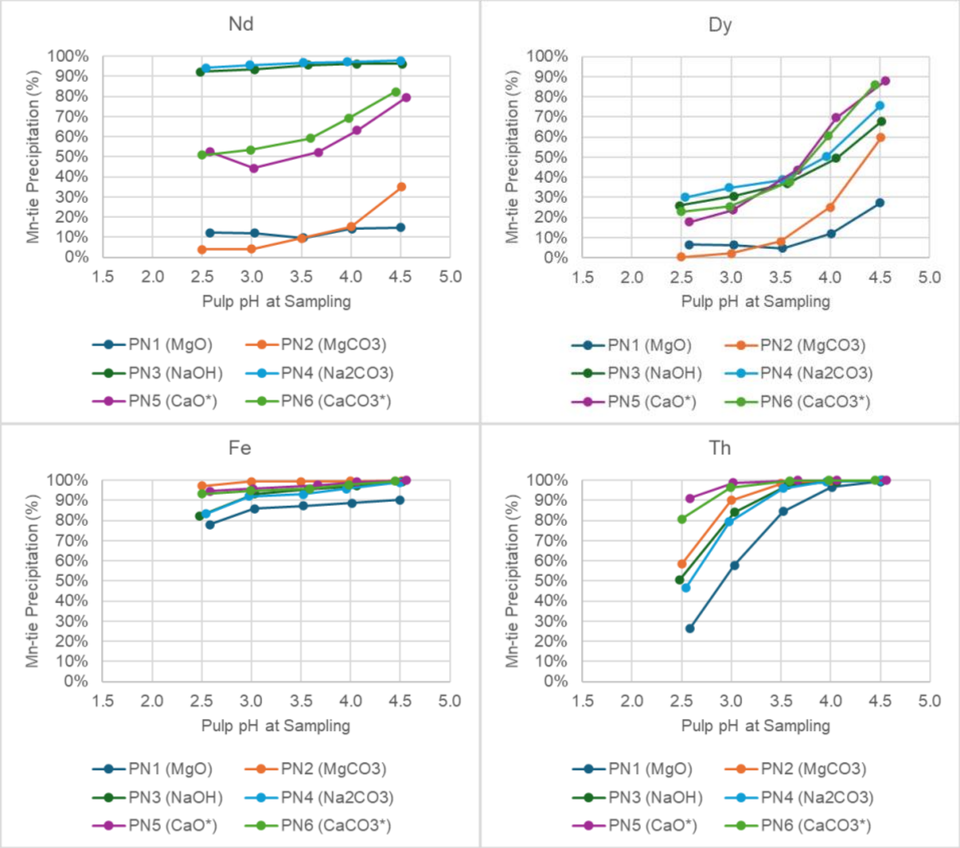
* client supplied sample

Precipitation (%)[1]	**PN1**	**PN2**	**PN3**	**PN4**	**PN5**	**PN6**
LREE Avg	5.3	21.6	60.6	74.1	68.0	71.6
HREE Avg	12.8	42.2	57.2	65.4	81.6	78.8
Th	90.3	97.5	94.4	92.8	99.1	98.1
U	52.0	84.4	72.7	77.8	98.4	96.4
Si	95.2	96.3	96.5	96.2	98.0	98.0
Al	80.4	92.0	82.1	81.3	93.2	89.3
Fe	87.2	99.5	96.9	96.0	98.9	98.1
Mg	0.1	0.1	2.1	3.3	21.5	10.3
Ca	0.5	0.7	4.1	11.2	96.9	96.7
Na	4.7	0.8	0.2	1.0	35.0	50.2
K	1.2	0.7	2.0	3.5	7.9	14.8
Ti	99.9	100.0	100.0	100.0	100.0	100.0
P	92.4	91.2	92.6	92.6	93.4	93.4
Mn	1.2	1.6	1.5	1.5	6.8	6.5

[1] overall, potentially skewed by partial sampling

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
		 Magnesium oxide (MgO) was selected as the neutralizing agent over other neutralizing agents due to low REE losses, impurity removal and cost. The pH adjustment and precipitation will be carried out in a cascade of stirred tank reactors with a combined residence time of 2 hrs. MgO will be purchased as a dry material

Section 3 Estimation and Reporting of Mineral Resources		
(Criteria listed in the preceding section also apply to this section.)		
Criteria	***JORC Code explanation***	**Commentary**
		and slaked onsite to form a 15% $Mg(OH)_2$ suspension which will be added to the tanks using a pH control loop. For the purposes of the mass balance and estimated MgO usage a ratio of 2.3% w/w for MgO (dry basis)/Leach PLS has been used based on laboratory testing. The solids generated by the iron removal step will be thickened in a cone bottom clarifier and filtered using a vacuum belt filter. The solids will be washed with water on the filter to minimize REE yield loss and disposed of.

Criteria	JORC Code explanation	Commentary

Test ID	PN10	PN9	PN13	PN7
Feed	Comp Bench AL Filtrate	Comp Bench AL Filtrate	AL22 Filtrate	Comp Bench AL Filtrate
Reagent	MgO	MgO	MgO	MgO
Reagent Strength (% w/w)	15%	15%	15%	15%
pH Target	2.75	3.00	3.15	3.25
Retention Time (h)[1]	3	3	1	2
Temperature (°C)	75	75	75	75
Reagent Addition (kg/m^3)	14.2	12.5	28	15
Est. Filtration Rate (kg/m^2h)	4.5	4.4	0.8	1.9

Precipitation (%)	PN10	PN9	PN13	PN7
LREE Avg	0.9	0.4	1.2	0.6
HREE Avg	1.0	0.6	2.1	1.5
Th	66.7	83.6	94.0	95.0
U	7.1	13.9	31.5	23.6
Si	88.4	91.7	94.8	92.1
Al	29.4	39.0	59.5	57.3
Fe	98.5	91.1	93.5	90.8
Mg	0.4	0.1	0.2	0.1
Ca	0.4	0.1	1.4	0.4
Na	4.9	3.7	4.5	3.4
K	0.9	0.4	1.5	0.5
Ti	98.1	99.1	99.5	99.6
P	89.8	89.9	92.8	89.3
Mn	1.1	1.1	1.2	1.1

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	**JORC Code explanation**	**Commentary**

Primary Neutralization

Test ID	**PN11**	**PN13**
Feed	AL22 Filtrate	AL22 Filtrate
Reagent	MgO	MgO
Reagent Strength (% w/w)	15%	15%
pH Target	3.15	3.15
Retention Time (h)[1]	2	1
Temperature (°C)	75	75
Reagent Addition (kg/m^3)	24	28
Est. Filtration Rate (kg/m^2h)	1.7	0.8

[1] for each pH target, as applicable

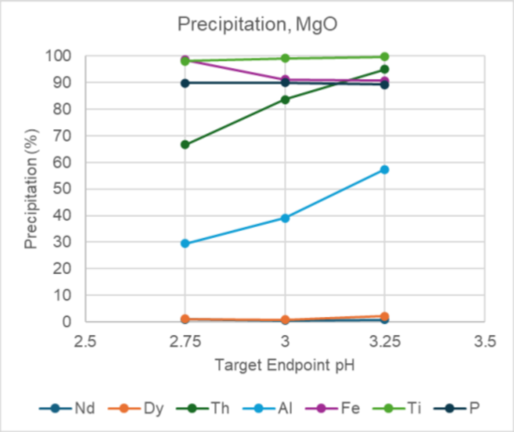
* client supplied sample

Precipitation (%)[1]	**PN11**	**PN13**
LREE Avg	3.2	1.2
HREE Avg	3.2	2.1
Th	92.2	94.0
U	39.1	31.5
Si	94.6	94.8
Al	43.2	59.5
Fe	95.9	93.5
Mg	1.1	0.2
Ca	42.5	1.4
Na	6.2	4.5
K	2.6	1.5
Ti	98.9	99.5
P	92.7	92.8
Mn	1.4	1.2

[1] overall, potentially skewed by partial sampling

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
		The Iron Removal step will operate at a pH of 3.15 and results in a near total removal of Fe, Th, Ti, and P along with partial removal of Al (approximately 50%) and U (approximately 20%) as can be seen in the Figure below. The partial removal of aluminium in the Iron Removal step is important since it will act as an outlet for aluminium to tailings as the Aluminium Removal (Al/U Removal) solids will be recycled back to leach in order to minimize REE loss.  **Secondary Neutralization** The Aluminum Removal consists of adding a neutralization agent (MgO) to increase the pH from 3.15, exiting the Iron Removal, to a pH of 5.0. The pH adjustment and resulting precipitation will be carried out in a cascade of stirred tank reactors with a combined residence time of 2 hrs and 75°C. MgO will be purchased as a dry material and slaked onsite to form a 15% $Mg(OH)2$ suspension which will be added to the tanks using a pH control loop. For the purposes of the mass balance and estimated MgO usage a ratio of 2.7% w/w for MgO (dry basis)/iron removal liquor has been used based on laboratory testing. The solids generated by the Secondary Neutralization will be thickened in a cone bottom clarifier and filtered using

Section 3 Estimation and Reporting of Mineral Resources		
(Criteria listed in the preceding section also apply to this section.)		
Criteria	***JORC Code explanation***	**Commentary**
		a vacuum belt filter. These solids will be recycled back to the leach circuit to reclaim any REE that co-precipitated. Rejection of aluminum and uranium will be in the iron removal solids.

Secondary Neutralization

Test ID	SN1	SN2	SN3
Feed	PN11 Filtrate	PN11 Filtrate	PN11 Filtrate
Reagent	MgO	MgO	MgO
Reagent Strength (% w/w)	15%	5-10%	5-10%
pH Target	4 - 6	5.00	5.25
Retention Time (h)1	1	2	2
Temperature (°C)	75	75	75
Reagent Addition (kg/m3)	3	3	3
Est. Filtration Rate (kg/m2h)	4.8	5.1	5.8

1 for each pH target, as applicable

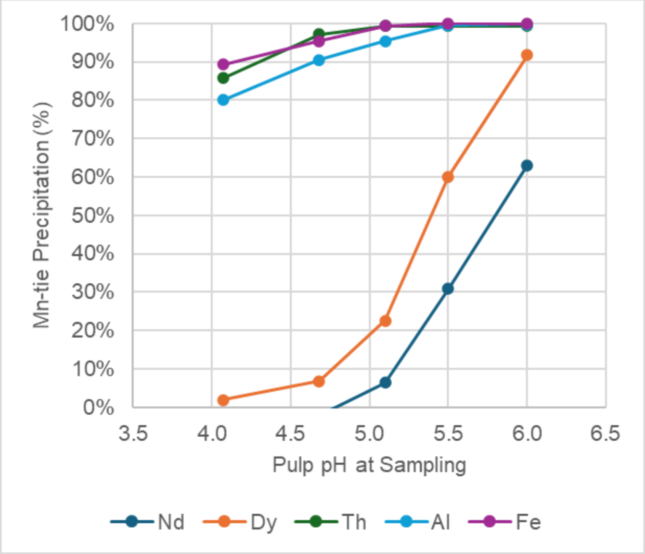
* client supplied sample

Precipitation (%)[1]	SN1	SN2	SN3
LREE Avg	49.1	7.6	12.3
HREE Avg	81.9	16.7	28.5
Th	98.1	98.9	98.9
U	81.6	19.8	36.3
Si	95.2	71.0	72.6
Al	96.7	96.3	99.5
Fe	98.5	99.4	99.6
Mg	1.1	0.1	0.2
Ca	1.4	0.3	0.5
Na	1.2	0.6	0.6
K	0.4	0.1	0.1
Ti	99.4	95.6	97.1
P	14.4	10.4	11.6
Mn	2.9	0.3	0.7
Zn	-	-	-

1. Overall, potentially skewed by partial sampling

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	*JORC Code explanation*	Commentary
		
Environmental factors or assumptions	*Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual*	ARR acquired exploration drilling notices from the Wyoming Department of Environmental Quality (WDEQ), Land Quality Division, for all drilling activities performed to date. ARR is developing a permitting needs assessment with local environmental consulting groups to present to each division at WDEQ to identify comprehensive environmental baseline studies needed to permit a mining operation at Halleck Creek. ARR is identifying additional regulatory stakeholders in Wyoming as part of the needs assessment. Factors for mine closure have been included in mining costs and financial modeling. At this stage of development, no mine closure plans have been developed. At this stage in project development, no social impact studies have been completed.

Criteria	***JORC Code explanation***	**Commentary**
	economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.	

Section 3 Estimation and Reporting of Mineral Resources		
(Criteria listed in the preceding section also apply to this section.)		
Criteria	***JORC Code explanation***	**Commentary**
Bulk density	*Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.* *Discuss assumptions for bulk density estimates used in the evaluation process of*	An average specific gravity of 2.70 represents the in-place ore material at Halleck Creek based on hydrostatic testing. Bulk density testing will be included during bulk sample collection currently being designed and permitted.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)

Criteria	***JORC Code explanation***	**Commentary**
	the different materials.	
Classification	*The basis for the classification of the Mineral Resources into varying confidence categories.* *Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* *Whether the result appropriately reflects the Competent Person's view of the deposit.*	The classification at Halleck Creek is based on the following key attributes: **Geological continuity between drill holes** • Mineralization is controlled by batholith-scale fractionation. Hence, both empirical observations and statistical analysis confirm a very high degree of continuity with the respective rock masses at Overton Mountain and Red Mountain. • This is supported by variography. **Drill spacing and drill density** • The drill pattern is mostly irregular with drill spacing of approximately 200m. • At Overton Mountain an area has been infilled on a systematic grid spacing of approximately 90m. This spacing is considered to be adequate to support a measured classification. • Drill hole spacing at Red Mountain is considered to be adequate to support indicated resources. The CP considers the above classification strategy and methodology to be appropriate and reasonable for this style of mineralisation.

Section 3 Estimation and Reporting of Mineral Resources		
(Criteria listed in the preceding section also apply to this section.)		
Criteria	***JORC Code explanation***	**Commentary**
Audits or reviews	*The results of any audits or reviews of Mineral Resource estimates.*	There have not been any audits of mineral resource estimates.
Discussion of relative accuracy/ confidence	*Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could*	Reported resources for Halleck Creek are in-place global estimates of tonnage and rare earth grade. The basis of classification of mineral resources was based on geostatistical analysis of variograms of rare earth elements. The resource is classified as either measured, indicated or inferred. Subject to the application of 'modifying factors' the measured plus indicated component of the resource may allow for a formal evaluation of its economics with the potential to be converted to a Probable Ore Reserve. Therefore, a high degree of conservatism has been adopted as the underlying premise of the resource classification and, in particular, the indicated component.

Criteria	***JORC Code explanation***	**Commentary**
	affect the relative accuracy and confidence of the estimate. *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	

SECTION 4 ESTIMATION AND REPORTING OF ORE RESERVES – ORE RESERVES ARE NOT BEING REPORTED